



1/98 IMOS WORKSHOP

presentation by

Andy Kissil

Jet Propulsion Laboratory

California Institute of Technology





Presentation Outline

- **# Overview of Using IMOS with NGST**
- **#** Identification of NGST Model Components
- **# Model Simplification**
- **# NGST 6/97 Model Overview**
- **# Model Checkout Results**
- **# Thermal Distortion Analysis**
- # Using Substructuring for Very Large Models
- **Summary of IMOS Experience with NGST**





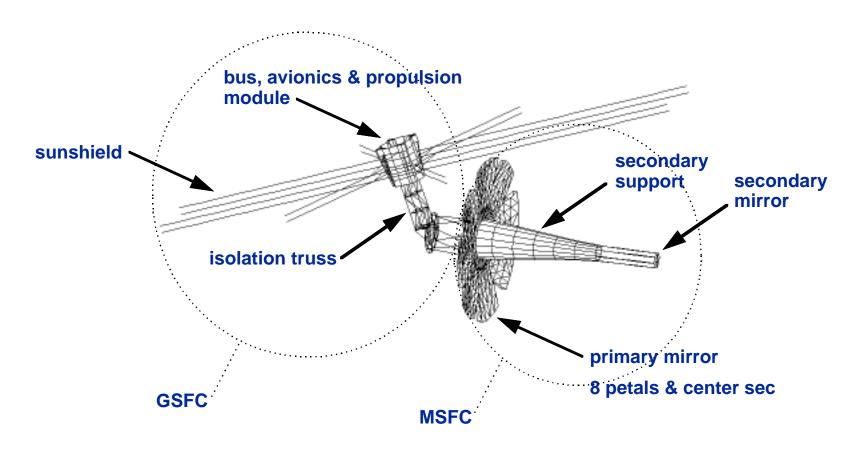
Overview of Using IMOS with NGST (structures):

- Conversion of Integrated NGST NASTRAN Model to IMOS
 - initial model simplification of GSFC S/C structure (in NASTRAN)
 - conversion using nas2imos (generates k and m)
- Eigenvalue Analysis
 - first 100 modes (using speig)
 - animation of mode shapes (using movmak/movply)
 - mode identification using modal strain and kinetic energies
- Generation of Modal State Space Models
 - assembly of a, b, c, d Matrices (using mode2ss)
- Thermal Distortion of Telescope due to Temperature Profile (from MSFC)
 - using thermal analysis script (see viewgraph)
- Transient Time History Dynamic Simulation (fhist from GSFC)
 - using Isim
 - animation of response (using movmak/movply)
- Parametric Studies of Stiffness Characteristics





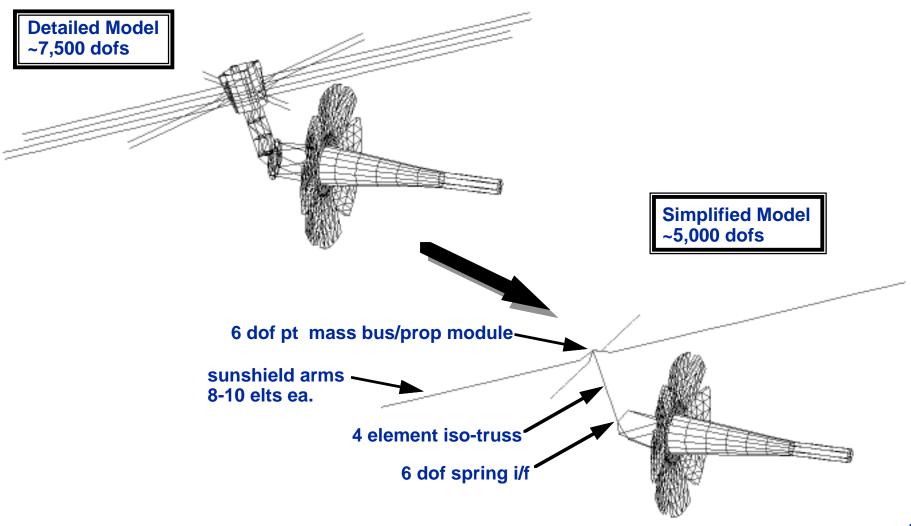
Identification of NGST Model Components







Model Simplification







NGST 6/97 Model Overview

Nodes: 904 Total

- 5060 Independent Dynamic dofs

Elements: 1335 Total

- beam 485

- conm 134

- celas 6

- plate 648

- rbe2 62

- **# Local Coordinate Systems: 12 Total**
 - 1 Spherical
 - 1 Cylindrical
 - 10 Rectangular
- # Plate Bending and Shear Factors (and Materials) Used in NASTRAN Model
 - Representing Honeycomb Sandwich Construction
 - Automatic Conversion Using nas2imos





Model Checkout Results

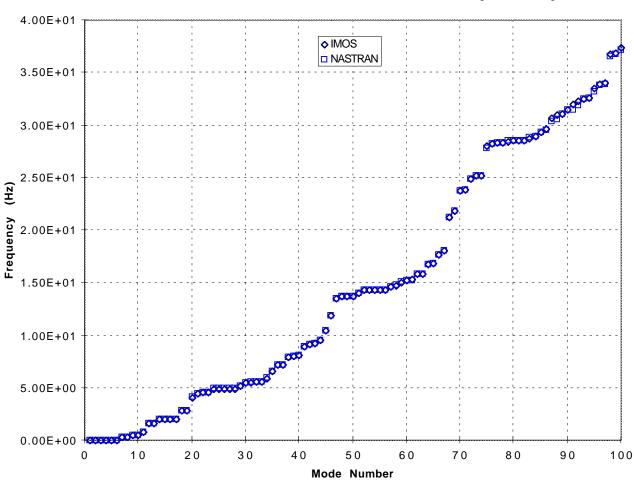
- # Rigid Body Mode Strain Energy Should be Small
 - automatic printout using rbmodesk
 - for NGST the largest component was found to be < 1.0e-7
- **#** Mass Properties Agree with NASTRAN
 - using wtcgk, cg_calck
 - Total mass= 2167 kg
 - Inertia Matrix about cg
 - Center of Gravity [xcg,ycg,zcg]= [-1.7050, -.02746, 1.4915]
- **# Normal Modes Analysis**
 - free-free boundary conditions (using speig with shifted k)
 - frequencies agree with NASTRAN (within 1%, see plot)
 - cross orthogonality of IMOS and NASTRAN modeshapes was good
 - ideally $\Phi_{\text{IMOS}}^{\ \ T} * M_{\text{IMOS}} * \Phi_{\text{NASTRAN}} = \text{I}$
 - found max diff of .01 on diagonal, max .10 off-diag (ave .0005 off-diag)
- # Transient Dynamic Analysis Response Agrees with NASTRAN (see plot)







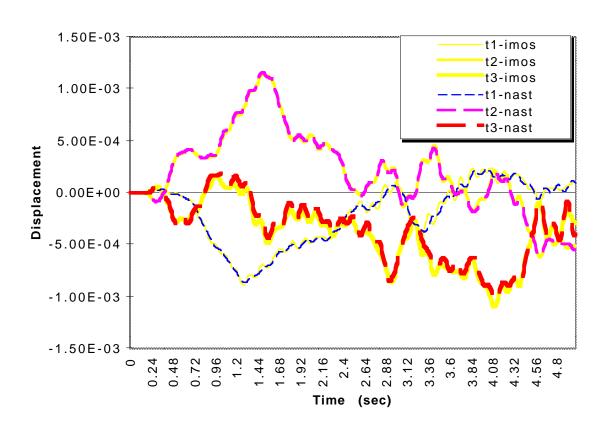
Comparison of Modal Frequencies for NASTRAN and IMOS Models (v.6/97)







Comparison of NASTRAN and IMOS Transient Response Histories







Thermal Distortion Analysis

- **#** Computed Mirror Distortion Vectors for Applied Temperature Profiles
 - Temperatures provided by MSFC in NASTRAN bulk data format
 - converted to IMOS automatically with nas2imos
 - Steady State Ground to Orbit (used 100 deg K ref)
 - used cte's integrated over temp range
 - subtract ref temp to get delta T
 - Thermal Transient, 1 hr slew with 27 hr hold (43 time steps)
 - no dynamics involved- static response only
 - temps at T=0 used as reference
 - used tplate and tbeam (see viewgraph)
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- **#** Compared Thermal Distortions from IMOS with NASTRAN
 - difference is much less than 1%, $(norm(u_{IMOS} u_{NASTRAN}) / norm(u_{NASTRAN}))$
- # Thermal Distortion Vectors Transmitted for Optical Performance Analysis





Script for Thermal Distortion Analysis

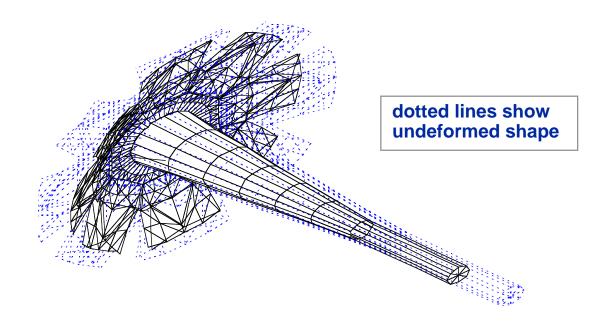
```
% This is a script to compute the displacement vector due to
% a temperature distribution (T) or gta.
niplate=[niquad; nitria];
ftoplate=tplate(niplate, xyz, propplt, mat, [1:length(niplate(:,1))]');
% ftobar=tbeam(nibar, xyz, propbar, [1:length(nibar(:,1))]');
ftobar=tbeam(nibar, xyz, propbar, [1:length(xyz(:, 1))]');
% Use Element temperatures
% etplate=tempvec(niplate, xyz, gta, 0.0);
% [etbar, nt]=tempvec(nibar, xyz, gta, 0.0);
% pgb=ftoplate*etplate + ftobar*etbar;
% pgb=ftoplate*etplate + ftobar*nt;
% Use Nodal temperatures- tn2e transforms nodal to elem temps
tn2e=tnode2el(niplate,xyz);
fto=ftoplate*tn2e + ftobar;
pgb=fto*T;
% transform thermal equiv forces from basic to local
t=gentloc(ti,tf);
pgl=t*pgb;
% reduce to nset and fset
if exist('gm')
 pgl(nset,:)=pgl(nset,:) + gm'*pgl(mset,:);
end
pfl=pgl(fset,:);
% compute displacements
phitl=k\pfl;
%phitl=pinv(full(k))*pfl;
% expand to gset
[np, mp]=size(phitl);
phigl=zeros(max(size(xyz))*6,mp);
phigl(fset,:)=phitl;
if exist('gm')
 phigl(mset,:)=gm*phigl(nset,:);
end
% transform to basic
phigb=t'*phigl;
```

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Plot of Thermal Distortion Steady State, Ground to Orbit







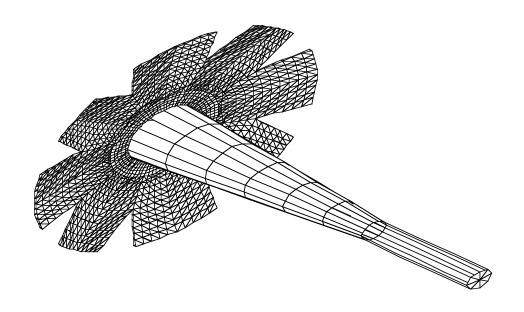
Using Substructuring for Very Large Models

- **# NGST Model with Deformable Glass Primary Mirror has 20,550 dofs**
 - Fine mesh required to capture actuator/structure interaction (448 actuators)
 - 36 actuators per petal (8 petals)
 - 160 actuators for central segment
 - Primary mirror model was already simplified
 - actuator spacing increased
- **"Out of memory "when trying to solve large eigenproblem**
- **# Substructuring offered solution**





NGST Telescope Model with Glass Primary (v.10/97)







Using Substructuring for Very Large Models

- # Implemented Substructuring- using Craig Bampton method
 - divided the structure into 6 parts, taking advantage of symmetry
 - central segment pie section (192 boundary dofs)
 - found that whole central segment was too big- 6738 dofs
 - used 1/8 pie section- 924 dofs for eigenproblem
 - petal type 1 (24 boundary dofs) (1584 dofs for eigenproblem)
 - petal type 2 (24 boundary dofs) (1584 dofs for eigenproblem)
 - secondary mirror & support structure (96 boundary dofs)
 - science instrumentation assembly (6 boundary dofs)
 - isolation truss, bus/prop module & sunshield (9 boundary dofs)
 - used cms comp cb.m to perform analysis on each of the 6 parts (see viewgraph)
 - compute fixed interface normal modes (eigenvalue analysis)
 - compute constraint modes (static)





Using Substructuring for Very Large Models

Script to generate component mode data for petal type 1 substructure

```
echo on
% define internal i-set and boundary b-set grid groups
ig1=[561:692,2177:2241,2243:2308];
ig1=[ig1' ones(length(ig1),6)];
bg1=[2097 1 1 1 0 0 0
  2102 1 1 1 1 1 1
   2107 1 1 1 0 0 0
   2242 1 1 1 1 1 1
  3166 1 1 1 1 1 1 1;
% get active internal and boundary dofs
is1=getdofs(ig1,xyz,bc);
bs1=getdofs(bg1,xyz,bc);
[knn1,kbb1,mnb1,mbb1,p1]=cms_comp_cb(k,m,is1,bs1,100);
% expand p to include dependent dofs, exclude spcs
[p1]=cms comp i2d(xyz,p1,ig1,is1,bs1,fset,spcgid,nset,mset,gm);
save petal_1c_cms knn1 kbb1 mnb1 mbb1 p1
```

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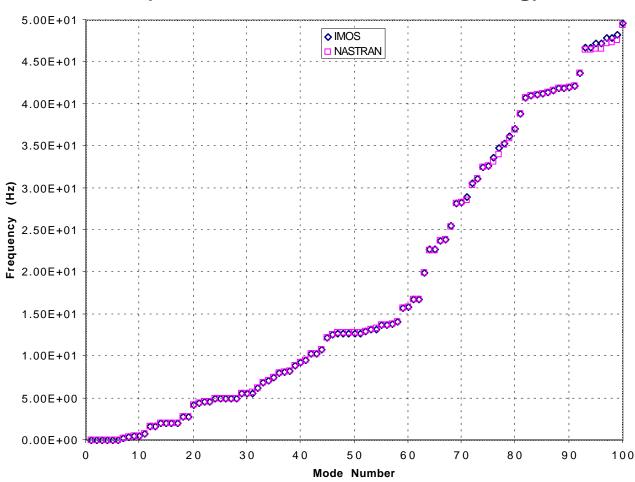
Using Substructuring for Very Large Models

- # Implemented Substructuring- using Craig Bampton method (cont'd)
 - replicated central segment pie section 8 times
 - replicated petal types 1 & 2 4 times each
 - total of 19 components assembled (including replications)
 - resulting system eigenproblem size of 2715 dofs
- # Comparison of resulting system frequencies between NASTRAN and IMOS
 - frequencies match within 1% (see plot)





Comparison of Modal Frequencies for NASTRAN and IMOS Models (Glass v. 10/97) (IMOS model used Substructuring)







Summary of IMOS Experience with NGST

- # Eigenvalue Analysis
 - speig sparse eigenvalue solver is slow for large problems
 - compiled version would help greatly
 - routine specializing in real-symmetric matrices would help too
 - have had bad results with small problems (< 1k dofs)
 - good results for large problems
 - need to check results
 - compute residuals from the modal equation
 - $\Re = K\Phi M\Phi\Lambda$
 - compare norm of each modal residual vector with that of $\,\mathrm{K}\Phi$
 - can recompute modes in problem frequency range
 - check orthogonality, i.e. $\Phi^{\mathrm{T}}\!\mathrm{M}\Phi$
 - can re-orthogonalize using onormphi (Gram-Schmidt) or other
 - sometimes small imaginary parts show up
 - can take real part if imaginary part is small enough
 - re-orthogonalize using onormphi





Summary of IMOS Experience with NGST (contd)

- # Thermal Distortion Analysis
 - need to re-check model after every modification
 - uniform cte with constant delta T (common sense, but ...)
- # Substructuring
 - tedious up front bookkeeping, but effective method
 - subsequent studies using mat changes would be fast
 - checking results of system eigen-analysis is essential (see prev viewgraph)
 - had to zero in on problem fequency ranges with speig
 - can use it for statics as well- just using constraint modes
- # Overall
 - favorable comparisons between IMOS and NASTRAN
 - flexibility of working in a MATLAB environment accelerates productivity
 - better eigen-solver would be a big help